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## Structure Reports

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## 4-Bromo- $N$-(4-bromophenyl)aniline

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Received 14 February 2011; accepted 24 February 2011
Key indicators: single-crystal X-ray study; $T=125 \mathrm{~K}$; mean $\sigma(\mathrm{C}-\mathrm{C})=0.003 \AA$; $R$ factor $=0.026 ; w R$ factor $=0.064 ;$ data-to-parameter ratio $=24.3$.

In the title compound, $\mathrm{C}_{12} \mathrm{H}_{9} \mathrm{Br}_{2} \mathrm{~N}$, the dihedral angle between the benzene rings is $47.32(5)^{\circ}$, whereas the pitch angles, or the angles between the mean plane of each aryl group 'propeller blade' and the plane defined by the aryl bridging $\mathrm{C}-\mathrm{N}-\mathrm{C}$ angle, are 18.1 (2) and 31.7 (2) ${ }^{\circ}$. No intermolecular $\mathrm{N}-\mathrm{H}$ hydrogen bonding is present in the crystal; however, there is a short intermolecular $\mathrm{Br} \cdots \mathrm{Br}$ contact of 3.568 (1) $\AA$.

## Related literature

The title compound is an amine analogue of brominated diphenyl ether flame retardant materials commonly used in household items. For information on environmental and health concerns related to brominated flame retardants, see: de Wit (2002); Lunder et al. (2010). For the synthesis of the title compound, see: Crounse \& Raiford (1945); Galatis \& Megaloikonomos (1934); He et al. (2008). For related structures, see: Eriksson et al. (2004); Plieth \& Ruban (1961); Li et al. (2010). For the van der Waals radius of Br and intermolecular $\mathrm{Br} \cdot$. Br contacts, see: Bondi (1964); Medlycott et al. (2007). For a description of the pitch angle, see: Lim \& Tanski (2007).


## Experimental

Crystal data
$\mathrm{C}_{12} \mathrm{H}_{9} \mathrm{Br}_{2} \mathrm{~N}$

$$
M_{r}=327.02
$$

Monoclinic, $P 2_{1} / c$
$a=5.9993$ (12) £
$b=13.032$ (3) $\AA$
$c=14.228$ (3) $\AA$
$\beta=96.967(3)^{\circ}$
$V=1104.2(4) \AA^{3}$

## Data collection

Bruker APEXII CCD
diffractometer
Absorption correction: multi-scan (SADABS; Bruker 2007)
$T_{\text {min }}=0.218, T_{\text {max }}=0.370$

## Refinement

$R\left[F^{2}>2 \sigma\left(F^{2}\right)\right]=0.026$
$w R\left(F^{2}\right)=0.064$
$S=1.02$
3373 reflections
139 parameters 1 restraint
$Z=4$
Mo $K \alpha$ radiation
$\mu=7.30 \mathrm{~mm}^{-1}$
$T=125 \mathrm{~K}$
$0.30 \times 0.30 \times 0.17 \mathrm{~mm}$

17275 measured reflections
3373 independent reflections 2786 reflections with $I>2 \sigma(I)$ $R_{\text {int }}=0.038$

H atoms treated by a mixture of independent and constrained refinement
$\Delta \rho_{\text {max }}=0.94 \mathrm{e}_{\AA^{-3}}$
$\Delta \rho_{\min }=-0.45 \mathrm{e}^{-3}$

Data collection: APEX2 (Bruker, 2007); cell refinement: SAINT (Bruker, 2007); data reduction: SAINT; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: SHELXTL (Sheldrick, 2008); software used to prepare material for publication: SHELXTL.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: SI2339).

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## supplementary materials

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## 4-Bromo- N -(4-bromophenyl)aniline

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## Comment

The title compound, 4-bromo- $N$-(4-bromophenyl)aniline, $\mathrm{C}_{12} \mathrm{H}_{9} \mathrm{Br}_{2} \mathrm{~N}$ (I), was first synthesized by Galatis \& Megaloikonomos (1934) via the direct bromination of diphenylamine, and the structure was corroborated by Crounse \& Raiford (1945) in their study of the hydrolysis of the benzoyl derivative. More recently, halogenated diphenylamines have been prepared by copper catalyzed coupling reactions (He et al., 2008). The crystal structure of the chloride analogue is known (Plieth \& Ruban, 1961), and an analogous structure with an oxygen bridge has also been reported (Eriksson et al., 2004). The title compound is an amine analogues of a class of brominated diphenyl ether materials (de Wit, 2002). Polybrominated diphenyl ethers are commonly used as flame retardants (Eriksson et al., 2004) in consumer products and electronics and have been found in humans (Lunder et al., 2010).

Compound (I) is a dibrominated diphenyl amine derivative with a "propeller blade" disposition of the benzene rings about the bridging nitrogen atom. The structure reveals that there is no intermolecular hydrogen bonding, although there are significant intermolecular $\mathrm{Br} \cdots \mathrm{Br}$ contacts (Medlycott et al. , 2007) at a distance of 3.568 (1) $\AA$, which is shorter than the sum of the van der Waals radius of bromine, $1.85 \AA$ (Bondi, 1964), at $3.7 \AA$. The aryl-bridging $\mathrm{C} 4 — \mathrm{~N} — \mathrm{C} 7$ angle in (I) is $128.5(2)^{\circ}$, somewhat smaller than the $\mathrm{C}-\mathrm{N}-\mathrm{C}$ bond angle of $133.8^{\circ}$ found in the isomorphous dichloro analog (Plieth \& Ruban, 1961), but similar to the $\mathrm{C}-\mathrm{N}-\mathrm{C}$ bond angle of $128.1^{\circ}$ in another similar structure, $N-4$-(bromophenyl)-4-nitroaniline, which contains one bromo and one nitro group (Li et al., 2010).

The dihedral angle in $(\mathrm{I})$ is found to be $47.32(5)^{\circ}$, whereas the pitch angles are $18.1(2)^{\circ}$ and $31.7(2)^{\circ}$. The pitch angles are the angles between the mean plane of each aryl group "propeller blade" and the plane defined by the aryl bridging $\mathrm{C} 4-\mathrm{N}-\mathrm{C} 7$ angle. The pitch angles are metrical parameters that describe the dispostion of the benzene rings about the bridging atom with greater detail than the dihedral angle; structures with equivalent dihedral angles may exhibit dramatically different orientations of the benzene rings about the bridging group (Lim \& Tanski, 2007). In the isomorphous dichloro analog to the title compound, the dihedral angle is found to be significantly larger, $56.5^{\circ}$, as are the pitch angles of $22.1^{\circ}$ and $39.1^{\circ}$. In another similar bromo compound, $N$-4-(bromophenyl)-4-nitroaniline, where the dihedral angle of $44.8^{\circ}$ is more similar to that of the title compound, the pitch angles are found to be $12.6^{\circ}$ and $35.1^{\circ}$.

## Experimental

Crystalline 4-bromo- N -(4-bromophenyl)aniline (I) was purchase from Aldrich Chemical Company, USA.

## Refinement

All non-hydrogen atoms were refined anisotropically. The hydrogen atoms on carbon were included in calculated positions and were refined using a riding model at $\mathrm{C}-\mathrm{H}=0.95 \AA$ and $U_{\mathrm{iso}}(\mathrm{H})=1.2 \times U_{\mathrm{eq}}(\mathrm{C})$ of the aryl C-atoms. T hydrogen atom on nitrogen was refined semifreely with the help of a distance restraint, $\mathrm{d}(\mathrm{N}-\mathrm{H})=0.835(16) \AA$ and $U_{\text {iso }}(\mathrm{H})=1.2 \times U_{\text {eq }}(\mathrm{N})$. The extinction parameter (EXTI) refined to zero and was removed from the refinement.

## supplementary materials

## Figures



Fig. 1. A view of compound (I), with displacement ellipsoids shown at the $50 \%$ probability level.

## 4-Bromo- N -(4-bromophenyl)aniline

## Crystal data

## $\mathrm{C}_{12} \mathrm{H}_{9} \mathrm{Br}_{2} \mathrm{~N}$

$M_{r}=327.02$
Monoclinic, $P 2_{1} / c$
Hall symbol: -P 2 ybc
$a=5.9993$ (12) $\AA$
$b=13.032$ (3) $\AA$
$c=14.228(3) \AA$
$\beta=96.967$ (3) ${ }^{\circ}$
$V=1104.2$ (4) $\AA^{3}$
$Z=4$
$F(000)=632$
$D_{\mathrm{x}}=1.967 \mathrm{Mg} \mathrm{m}^{-3}$
Mo $K \alpha$ radiation, $\lambda=0.71073 \AA$
Cell parameters from 8371 reflections
$\theta=2.9-30.4^{\circ}$
$\mu=7.30 \mathrm{~mm}^{-1}$
$T=125 \mathrm{~K}$
Plate, colourless
$0.30 \times 0.30 \times 0.17 \mathrm{~mm}$

## Data collection

## Bruker APEXII CCD

diffractometer
Radiation source: fine-focus sealed tube
graphite
$\varphi$ and $\omega$ scans
Absorption correction: multi-scan
(SADABS; Bruker 2007)
$T_{\text {min }}=0.218, T_{\text {max }}=0.370$
17275 measured reflections

## Refinement

## Refinement on $F^{2}$

Least-squares matrix: full
$R\left[F^{2}>2 \sigma\left(F^{2}\right)\right]=0.026$
$w R\left(F^{2}\right)=0.064$
$S=1.02$
3373 reflections
139 parameters

Primary atom site location: structure-invariant direct methods
Secondary atom site location: difference Fourier map
Hydrogen site location: inferred from neighbouring sites
H atoms treated by a mixture of independent and constrained refinement
$w=1 /\left[\sigma^{2}\left(F_{\mathrm{o}}{ }^{2}\right)+(0.0365 P)^{2}\right]$
where $P=\left(F_{\mathrm{o}}^{2}+2 F_{\mathrm{c}}^{2}\right) / 3$
$(\Delta / \sigma)_{\max }=0.001$
$\Delta \rho_{\text {max }}=0.94 \mathrm{e} \AA^{-3}$

1 restraint

$$
\Delta \rho_{\min }=-0.45 \mathrm{e} \AA^{-3}
$$

## Special details

Experimental. A suitable crystal was mounted in a nylon loop with Paratone-N cryoprotectant oil and data was collected on a Bruker APEX 2 CCD platform diffractometer. The structure was solved using direct methods and standard difference map techniques, and was refined by full-matrix least-squares procedures on $\mathrm{F}^{2}$ with SHELXTL Version 6.14 (Sheldrick, 2008).
Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two 1.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving 1.s. planes.

Refinement. Refinement of $F^{2}$ against ALL reflections. The weighted $R$-factor $w R$ and goodness of fit $S$ are based on $F^{2}$, conventional $R$-factors $R$ are based on $F$, with $F$ set to zero for negative $F^{2}$. The threshold expression of $F^{2}>\sigma\left(F^{2}\right)$ is used only for calculating $R$ factors(gt) etc. and is not relevant to the choice of reflections for refinement. $R$-factors based on $F^{2}$ are statistically about twice as large as those based on $F$, and $R$ - factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters ( $A^{2}$ )

|  | $x$ | $y$ | $z$ | $U_{\text {iso }}{ }^{*} / U_{\text {eq }}$ |
| :--- | :--- | :--- | :--- | :--- |
| Br1 | $0.35642(4)$ | $0.125752(16)$ | $0.143618(15)$ | $0.02649(7)$ |
| Br 2 | $-0.19656(3)$ | $0.946875(15)$ | $0.134200(15)$ | $0.02372(7)$ |
| N | $0.4407(3)$ | $0.58823(13)$ | $0.10486(13)$ | $0.0224(4)$ |
| H 1 | $0.566(3)$ | $0.6043(18)$ | $0.0893(16)$ | $0.027^{*}$ |
| C1 | $0.3790(3)$ | $0.27103(16)$ | $0.13498(13)$ | $0.0200(4)$ |
| C2 | $0.5839(3)$ | $0.31866(15)$ | $0.16241(14)$ | $0.0229(4)$ |
| H2A | 0.7114 | 0.2793 | 0.1865 | $0.027^{*}$ |
| C3 | $0.5998(3)$ | $0.42427(15)$ | $0.15413(14)$ | $0.0215(4)$ |
| H3A | 0.7391 | 0.4573 | 0.1733 | $0.026^{*}$ |
| C4 | $0.4131(3)$ | $0.48316(15)$ | $0.11792(13)$ | $0.0186(4)$ |
| C5 | $0.2092(3)$ | $0.43296(15)$ | $0.09209(14)$ | $0.0204(4)$ |
| H5A | 0.0806 | 0.4719 | 0.0685 | $0.025^{*}$ |
| C6 | $0.1911(3)$ | $0.32763(15)$ | $0.10030(14)$ | $0.0209(4)$ |
| H6A | 0.0514 | 0.2944 | 0.0824 | $0.025^{*}$ |
| C7 | $0.2844(3)$ | $0.66694(15)$ | $0.10980(14)$ | $0.0188(4)$ |
| C8 | $0.0933(3)$ | $0.65683(15)$ | $0.15638(14)$ | $0.0192(4)$ |
| H8A | 0.0621 | 0.5931 | 0.1845 | $0.023^{*}$ |
| C9 | $-0.0513(3)$ | $0.73940(15)$ | $0.16173(13)$ | $0.0194(4)$ |
| H9A | -0.1822 | 0.7318 | 0.1925 | $0.023^{*}$ |
| C10 | $-0.0044(3)$ | $0.83266(14)$ | $0.12218(14)$ | $0.0191(4)$ |
| C11 | $0.1859(3)$ | $0.84517(15)$ | $0.07631(14)$ | $0.0208(4)$ |
| H11A | 0.2179 | 0.9096 | 0.0497 | $0.025^{*}$ |
| C12 | $0.3281(3)$ | $0.76224(15)$ | $0.06992(13)$ | $0.0202(4)$ |
| H12A | 0.4572 | 0.7701 | 0.0380 | $0.024^{*}$ |

Atomic displacement parameters $\left(A^{2}\right)$
$U^{11} \quad U^{22}$
$U^{33} \quad U^{12}$
$U^{13} \quad U^{23}$

|  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Br 1 | $0.03250(12)$ | $0.01599(11)$ | $0.03174(12)$ | $0.00176(8)$ | $0.00695(9)$ | $-0.00159(8)$ |
| Br 2 | $0.02408(11)$ | $0.01647(10)$ | $0.03091(12)$ | $0.00214(7)$ | $0.00456(8)$ | $-0.00193(7)$ |
| N | $0.0179(8)$ | $0.0174(8)$ | $0.0330(10)$ | $0.0004(7)$ | $0.0076(7)$ | $0.0013(7)$ |
| C 1 | $0.0219(9)$ | $0.0166(9)$ | $0.0217(9)$ | $0.0016(7)$ | $0.0039(7)$ | $-0.0020(7)$ |
| C 2 | $0.0197(9)$ | $0.0232(10)$ | $0.0253(10)$ | $0.0046(8)$ | $0.0008(8)$ | $0.0007(8)$ |
| C 3 | $0.0144(9)$ | $0.0215(10)$ | $0.0283(10)$ | $-0.0001(7)$ | $0.0012(7)$ | $-0.0016(8)$ |
| C4 | $0.0203(9)$ | $0.0182(9)$ | $0.0180(9)$ | $-0.0002(7)$ | $0.0051(7)$ | $-0.0009(7)$ |
| C5 | $0.0184(9)$ | $0.0210(10)$ | $0.0212(9)$ | $0.0031(7)$ | $-0.0006(7)$ | $-0.0014(7)$ |
| C6 | $0.0189(9)$ | $0.0225(10)$ | $0.0211(9)$ | $-0.0008(7)$ | $0.0020(7)$ | $-0.0033(7)$ |
| C7 | $0.0192(9)$ | $0.0167(9)$ | $0.0205(9)$ | $-0.0008(7)$ | $0.0019(7)$ | $0.0001(7)$ |
| C8 | $0.0204(9)$ | $0.0155(9)$ | $0.0219(9)$ | $-0.0030(7)$ | $0.0038(7)$ | $0.0002(7)$ |
| C9 | $0.0176(9)$ | $0.0207(10)$ | $0.0206(9)$ | $-0.0031(7)$ | $0.0049(7)$ | $-0.0008(7)$ |
| C10 | $0.0192(9)$ | $0.0150(9)$ | $0.0227(9)$ | $0.0017(7)$ | $0.0005(7)$ | $-0.0019(7)$ |
| C11 | $0.0239(10)$ | $0.0156(9)$ | $0.0232(10)$ | $-0.0042(7)$ | $0.0038(8)$ | $0.0009(7)$ |
| C12 | $0.0193(9)$ | $0.0210(9)$ | $0.0210(9)$ | $-0.0027(7)$ | $0.0049(7)$ | $-0.0007(7)$ |

Geometric parameters ( $\AA$, ${ }^{\circ}$ )

| $\mathrm{Br} 1-\mathrm{C} 1$ | $1.903(2)$ |
| :--- | :--- |
| $\mathrm{Br} 2-\mathrm{C} 10$ | $1.9031(19)$ |
| $\mathrm{N}-\mathrm{C} 4$ | $1.394(3)$ |
| $\mathrm{N}-\mathrm{C} 7$ | $1.397(3)$ |
| $\mathrm{N}-\mathrm{H} 1$ | $0.835(16)$ |
| $\mathrm{C} 1-\mathrm{C} 6$ | $1.387(3)$ |
| $\mathrm{C} 1-\mathrm{C} 2$ | $1.390(3)$ |
| $\mathrm{C} 2-\mathrm{C} 3$ | $1.386(3)$ |
| $\mathrm{C} 2-\mathrm{H} 2 \mathrm{~A}$ | 0.9500 |
| $\mathrm{C} 3-\mathrm{C} 4$ | $1.403(3)$ |
| $\mathrm{C} 3-\mathrm{H} 3 \mathrm{~A}$ | 0.9500 |
| $\mathrm{C} 4-\mathrm{C} 5$ | $1.397(3)$ |
| $\mathrm{C} 5-\mathrm{C} 6$ | $1.383(3)$ |
| $\mathrm{C} 4-\mathrm{N}-\mathrm{C} 7$ | $128.53(17)$ |
| $\mathrm{C} 4-\mathrm{N}-\mathrm{H} 1$ | $114.0(17)$ |
| $\mathrm{C} 7-\mathrm{N}-\mathrm{H} 1$ | $117.4(17)$ |
| $\mathrm{C} 6-\mathrm{C} 1-\mathrm{C} 2$ | $121.03(19)$ |
| $\mathrm{C} 6-\mathrm{C} 1-\mathrm{Br} 1$ | $119.41(15)$ |
| $\mathrm{C} 2-\mathrm{C} 1-\mathrm{Br} 1$ | $119.56(15)$ |
| $\mathrm{C} 3-\mathrm{C} 2-\mathrm{C} 1$ | $119.14(18)$ |
| $\mathrm{C} 3-\mathrm{C} 2-\mathrm{H} 2 \mathrm{~A}$ | 120.4 |
| $\mathrm{C} 1-\mathrm{C} 2-\mathrm{H} 2 \mathrm{~A}$ | 120.4 |
| $\mathrm{C} 2-\mathrm{C} 3-\mathrm{C} 4$ | $120.97(18)$ |
| $\mathrm{C} 2-\mathrm{C} 3-\mathrm{H} 3 \mathrm{~A}$ | 119.5 |
| $\mathrm{C} 4-\mathrm{C} 3-\mathrm{H} 3 \mathrm{~A}$ | 119.5 |
| $\mathrm{~N}-\mathrm{C} 4-\mathrm{C} 5$ | $122.64(18)$ |
| $\mathrm{N}-\mathrm{C} 4-\mathrm{C} 3$ | $118.93(17)$ |
| $\mathrm{C} 5-\mathrm{C} 4-\mathrm{C} 3$ | $118.36(18)$ |
| $\mathrm{C} 6-\mathrm{C} 5-\mathrm{C} 4$ | $121.20(18)$ |
| $\mathrm{C} 6-\mathrm{C} 5-\mathrm{H} 5 \mathrm{~A}$ | 119.4 |
| $\mathrm{C} 4-\mathrm{C} 5-\mathrm{H} 5 \mathrm{~A}$ | 119.4 |


| C5-H5A | 0.9500 |
| :---: | :---: |
| C6-H6A | 0.9500 |
| C7-C8 | 1.399 (3) |
| C7-C12 | 1.403 (3) |
| C8-C9 | 1.390 (3) |
| C8-H8A | 0.9500 |
| C9-C10 | 1.383 (3) |
| C9-H9A | 0.9500 |
| C10-C11 | 1.391 (3) |
| C11-C12 | 1.387 (3) |
| C11-H11A | 0.9500 |
| C12-H12A | 0.9500 |
| C1-C6-H6A | 120.4 |
| $\mathrm{N}-\mathrm{C} 7-\mathrm{C} 8$ | 123.26 (17) |
| $\mathrm{N}-\mathrm{C} 7-\mathrm{C} 12$ | 118.05 (17) |
| C8-C7-C12 | 118.62 (18) |
| C9-C8-C7 | 120.40 (18) |
| C9-C8-H8A | 119.8 |
| C7-C8-H8A | 119.8 |
| C10-C9-C8 | 119.93 (18) |
| C10-C9-H9A | 120.0 |
| C8-C9-H9A | 120.0 |
| C9-C10-C11 | 120.87 (18) |
| C9-C10-Br2 | 119.70 (15) |
| $\mathrm{C} 11-\mathrm{C} 10-\mathrm{Br} 2$ | 119.40 (14) |
| C12-C11-C10 | 119.05 (18) |
| C12-C11-H11A | 120.5 |
| $\mathrm{C} 10-\mathrm{C} 11-\mathrm{H} 11 \mathrm{~A}$ | 120.5 |
| C11-C12-C7 | 121.13 (18) |
| C11-C12-H12A | 119.4 |

## sup-4

## supplementary materials

| $\mathrm{C} 5-\mathrm{C} 6-\mathrm{C} 1$ | $119.28(19)$ |
| :--- | :--- |
| $\mathrm{C} 5-\mathrm{C} 6-\mathrm{H} 6 A$ | 120.4 |
| $\mathrm{C} 6-\mathrm{C} 1-\mathrm{C} 2-\mathrm{C} 3$ | $-0.5(3)$ |
| $\mathrm{Br}-\mathrm{C} 1-\mathrm{C} 2-\mathrm{C} 3$ | $178.75(15)$ |
| $\mathrm{C} 1-\mathrm{C} 2-\mathrm{C} 3-\mathrm{C} 4$ | $-0.5(3)$ |
| $\mathrm{C} 7-\mathrm{N}-\mathrm{C} 4-\mathrm{C} 5$ | $33.3(3)$ |
| $\mathrm{C} 7-\mathrm{N}-\mathrm{C} 4-\mathrm{C} 3$ | $-149.9(2)$ |
| $\mathrm{C} 2-\mathrm{C} 3-\mathrm{C} 4-\mathrm{N}$ | $-175.67(18)$ |
| $\mathrm{C} 2-\mathrm{C} 3-\mathrm{C} 4-\mathrm{C} 5$ | $1.3(3)$ |
| $\mathrm{N}-\mathrm{C} 4-\mathrm{C} 5-\mathrm{C} 6$ | $175.75(18)$ |
| $\mathrm{C} 3-\mathrm{C} 4-\mathrm{C} 5-\mathrm{C} 6$ | $-1.1(3)$ |
| $\mathrm{C} 4-\mathrm{C} 5-\mathrm{C} 6-\mathrm{C} 1$ | $0.1(3)$ |
| $\mathrm{C} 2-\mathrm{C} 1-\mathrm{C} 6-\mathrm{C} 5$ | $0.7(3)$ |
| $\mathrm{Br} 1-\mathrm{C} 1-\mathrm{C} 6-\mathrm{C} 5$ | $-178.55(14)$ |


| $\mathrm{C} 7-\mathrm{C} 12-\mathrm{H} 12 \mathrm{~A}$ | 119.4 |
| :--- | :--- |
| $\mathrm{C} 4-\mathrm{N}-\mathrm{C} 7-\mathrm{C} 8$ | $20.0(3)$ |
| $\mathrm{C} 4-\mathrm{N}-\mathrm{C} 7-\mathrm{C} 12$ | $-163.25(19)$ |
| $\mathrm{N}-\mathrm{C} 7-\mathrm{C} 8-\mathrm{C} 9$ | $177.59(18)$ |
| $\mathrm{C} 12-\mathrm{C} 7-\mathrm{C} 8-\mathrm{C} 9$ | $0.8(3)$ |
| $\mathrm{C} 7-\mathrm{C} 8-\mathrm{C} 9-\mathrm{C} 10$ | $-1.1(3)$ |
| $\mathrm{C} 8-\mathrm{C} 9-\mathrm{C} 10-\mathrm{C} 11$ | $0.4(3)$ |
| $\mathrm{C} 8-\mathrm{C} 9-\mathrm{C} 10-\mathrm{Br} 2$ | $-177.49(14)$ |
| $\mathrm{C} 9-\mathrm{C} 10-\mathrm{C} 11-\mathrm{C} 12$ | $0.5(3)$ |
| $\mathrm{Br} 2-\mathrm{C} 10-\mathrm{C} 11-\mathrm{C} 12$ | $178.40(15)$ |
| $\mathrm{C} 10-\mathrm{C} 11-\mathrm{C} 12-\mathrm{C} 7$ | $-0.8(3)$ |
| $\mathrm{N}-\mathrm{C} 7-\mathrm{C} 12-\mathrm{C} 11$ | $-176.84(18)$ |
| $\mathrm{C} 8-\mathrm{C} 7-\mathrm{C} 12-\mathrm{C} 11$ | $0.1(3)$ |

## supplementary materials

Fig. 1


